

# Dual and Quad 45MHz, 400V/µs Op Amps

# **FEATURES**

- 45MHz Gain-Bandwidth
- 400V/µs Slew Rate
- Unity-Gain Stable
- 7V/mV DC Gain,  $R_1 = 500\Omega$
- 3mV Maximum Input Offset Voltage
- $\pm 12$ V Minimum Output Swing into  $500\Omega$
- Wide Supply Range: ±2.5V to ±15V
- 7mA Supply Current per Amplifier
- 90ns Settling Time to 0.1%, 10V Step
- Drives All Capacitive Loads

# **APPLICATIONS**

- Wideband Amplifiers
- Buffers
- Active Filters
- Video and RF Amplification
- Cable Drivers
- Data Acquisition Systems

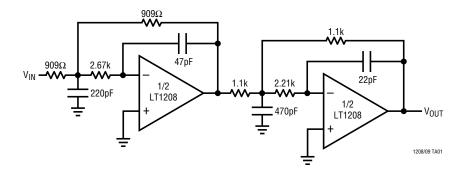
# DESCRIPTION

The LT1208/LT1209 are dual and quad very high speed operational amplifiers with excellent DC performance. The LT1208/LT1209 feature reduced input offset voltage and higher DC gain than devices with comparable bandwidth and slew rate. Each amplifier is a single gain stage with outstanding settling characteristics. The fast settling time makes the circuit an ideal choice for data acquisition systems. Each output is capable of driving a  $500\Omega$  load to  $\pm 12V$  with  $\pm 15V$  supplies and a  $150\Omega$  load to  $\pm 3V$  on  $\pm 5V$  supplies. The amplifiers are also capable of driving large capacitive loads which make them useful in buffer or cable driver applications.

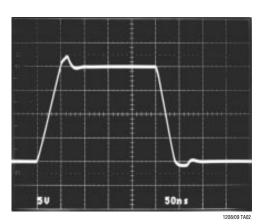
The LT1208/LT1209 are members of a family of fast, high performance amplifiers that employ Linear Technology Corporation's advanced bipolar complementary processing.

# TYPICAL APPLICATION

### 1MHz, 4th Order Butterworth Filter



### **Inverter Pulse Response**

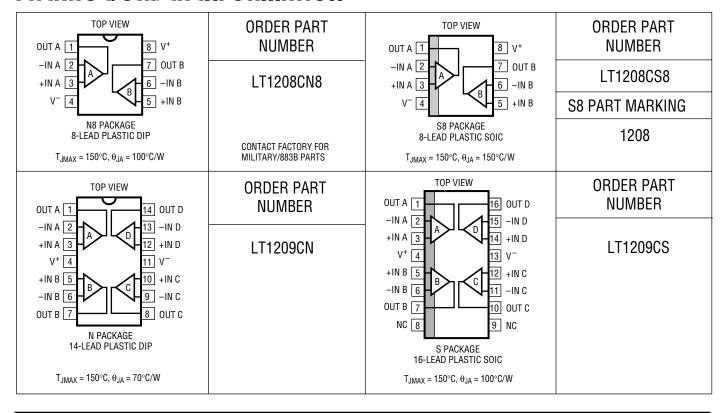


# **ABSOLUTE MAXIMUM RATINGS**

Total Supply Voltage (V <sup>+</sup> to V <sup>-</sup> )	36V
Differential Input Voltage	±6V
Input Voltage	±V <sub>S</sub>
Output Short-Circuit Duration (Note 1)	Indefinite
Operating Temperature Range	
LT1208C/LT1209C40°	C to 85°C

Maximum Junction Temperature	
Plastic Package 1	150°C
Storage Temperature Range – 65°C to 1	150°C
Lead Temperature (Soldering, 10 sec) 3	300°C

# PACKAGE/ORDER INFORMATION



# **ELECTRICAL CHARACTERISTICS** $v_{S}=\pm15V,\, T_{A}=25^{\circ}C,\, R_{L}=1k,\, V_{CM}=0V,\, unless \, otherwise \, noted.$

SYMBOL V <sub>OS</sub>	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
	Input Offset Voltage	$V_S = \pm 5V \text{ (Note 2)}$ 0°C to 70°C	•		0.5	3.0 4.0	mV mV
		$V_S = \pm 15V \text{ (Note 2)}$ 0°C to 70°C	•		1.0	5.0 6.0	mV mV
	Input V <sub>OS</sub> Drift				25		μV/°C
I <sub>0S</sub>	Input Offset Current	$V_S = \pm 5V$ and $V_S = \pm 15V$ 0°C to 70°C	•		100	400 600	nA nA
I <sub>B</sub>	Input Bias Current	$V_S = \pm 5V$ and $V_S = \pm 15V$ 0°C to 70°C	•		4	8 9	μA μA
e <sub>n</sub>	Input Noise Voltage	f = 10kHz			22		nV/√Hz
i <sub>n</sub>	Input Noise Current	f = 10kHz			1.1		pA/√Hz

# **ELECTRICAL CHARACTERISTICS** $v_{S}=\pm15V,\, T_{A}=25^{\circ}C,\, R_{L}=1k,\, V_{CM}=0V,\, unless \, otherwise \, noted.$

SYMBOL	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
R <sub>IN</sub>	Input Resistance	$V_{CM} = \pm 12V$		20	40		$M\Omega$
		Differential			250		kΩ
C <sub>IN</sub>	Input Capacitance				2		pF
CMRR	Common-Mode Rejection Ratio	$V_S = \pm 15V$ , $V_{CM} = \pm 12V$ ; $V_S = \pm 5V$ , $V_{CM} = \pm 2.5V$ , 0°C to 70°C	•	86 83	98		dB dB
PSRR	Power Supply Rejection Ratio	V <sub>S</sub> = ±5V to ±15V 0°C to 70°C	•	76 75	84		dB dB
	Input Voltage Range	$V_S = \pm 15V$ $V_S = \pm 5V$		±12 ±2.5	±13 ±3		V
A <sub>VOL</sub>	Large-Signal Voltage Gain	$V_S = \pm 15V$ , $V_{OUT} = \pm 10V$ , $R_L = 500\Omega$ 0°C to 70°C	•	3.3 2.5	7		V/mV V/mV
		$V_S = \pm 5V$ , $V_{OUT} = \pm 2.5V$ , $R_L = 500\Omega$ 0°C to 70°C	•	2.5 2.0	7		V/mV V/mV
		$V_S = \pm 5V$ , $V_{OUT} = \pm 2.5V$ , $R_L = 150\Omega$			3		V/mV
V <sub>OUT</sub>	Output Swing	$V_S = \pm 15V$ , $R_L = 500\Omega$ , 0°C to 70°C $V_S = \pm 5V$ , $R_L = 150\Omega$ , 0°C to 70°C	•	12.0 3.0	13.3 3.3		±V ±V
I <sub>OUT</sub>	Output Current	$V_S = \pm 15V$ , $V_{OUT} = \pm 12V$ , 0°C to 70°C $V_S = \pm 5V$ , $V_{OUT} = \pm 3V$ , 0°C to 70°C	•	24 20	40 40		mA mA
SR	Slew Rate	$V_S = \pm 15V$ , $A_{VCL} = -2$ , (Note 3) 0°C to 70°C	•	250 200	400		V/μs V/μs
		$V_S = \pm 5V$ , $A_{VCL} = -2$ , (Note 3) 0°C to 70°C	•	150 130	250		V/μs V/μs
	Full Power Bandwidth	10V Peak, (Note 4)			6.4		MHz
GBW	Gain-Bandwidth	$V_S = \pm 15V$ , f = 1MHz $V_S = \pm 5V$ , f = 1MHz			45 34		MHz MHz
t <sub>r</sub> , t <sub>f</sub>	Rise Time, Fall Time	$V_S = \pm 15V$ , $A_{VCL} = 1$ , 10% to 90%, 0.1V $V_S = \pm 5V$ , $A_{VCL} = 1$ , 10% to 90%, 0.1V			5 7		ns ns
	Overshoot	$V_S = \pm 15V$ , $A_{VCL} = 1$ , 0.1V $V_S = \pm 5V$ , $A_{VCL} = 1$ , 0.1V			30 20		% %
	Propagation Delay	$V_S = \pm 15V$ , 50% $V_{IN}$ to 50% $V_{OUT}$ $V_S = \pm 5V$ , 50% $V_{IN}$ to 50% $V_{OUT}$			5 7		ns ns
t <sub>s</sub>	Settling Time	$V_S = \pm 15V$ , 10V Step, $V_S = \pm 5V$ , 5V Step, 0.1%			90		ns
	Differential Gain	$f = 3.58MHz, R_L = 150\Omega$ $f = 3.58MHz, R_L = 1k$			1.30 0.09		% %
	Differential Phase	$f = 3.58MHz$ , $R_L = 150Ω$ $f = 3.58MHz$ , $R_L = 1k$			1.8 0.1		Deg Deg
$\overline{R_0}$	Output Resistance	A <sub>VCL</sub> = 1, f = 1MHz			2.5		Ω
	Crosstalk	$V_{OUT} = \pm 10V$ , $R_L = 500\Omega$			-100	-94	dB
Is	Supply Current	Each Amplifier, $V_S = \pm 5V$ and $V_S = \pm 15V$ 0°C to 70°C	•		7	9 10.5	mA mA

The ullet denotes the specifications which apply over the full operating temperature range.

**Note 1:** A heat sink may be required to keep the junction temperature below absolute maximum when the output is shorted indefinitely.

**Note 2:** Input offset voltage is tested with automated test equipment and is exclusive of warm-up drift.

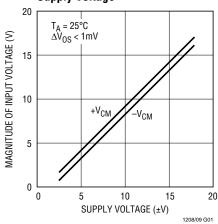
**Note 3:** Slew rate is measured in a gain of -2. For  $\pm 15V$  supplies measure between  $\pm 10V$  on the output with  $\pm 6V$  on the input. For  $\pm 5V$  supplies measure between  $\pm 2V$  on the output with  $\pm 1.75V$  on the input.

**Note 4:** Full power bandwidth is calculated from the slew rate measurement: FPBW =  $SR/2\pi V_P$ .

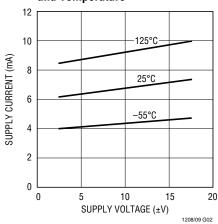


# TYPICAL PERFORMANCE CHARACTERISTICS

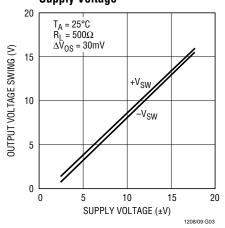




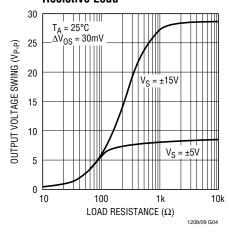
# **Supply Current vs Supply Voltage** and Temperature



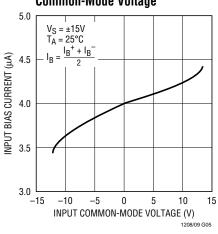
**Output Voltage Swing vs Supply Voltage** 



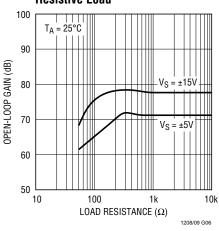
**Output Voltage Swing vs Resistive Load** 



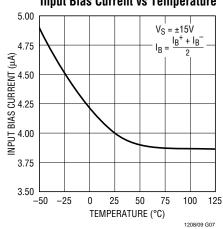
**Input Bias Current vs Input** Common-Mode Voltage



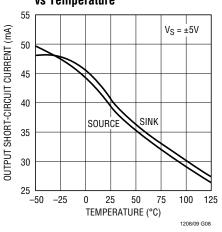
Open-Loop Gain vs Resistive Load



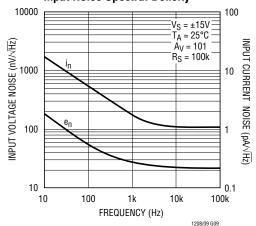
**Input Bias Current vs Temperature** 



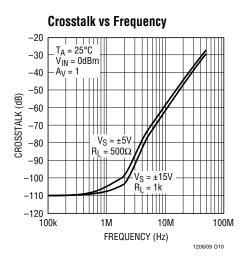
**Output Short-Circuit Current** vs Temperature

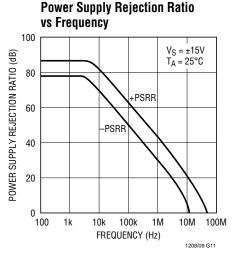


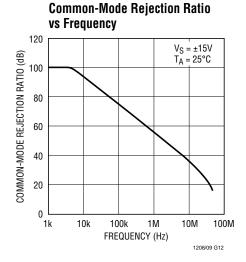
**Input Noise Spectral Density** 

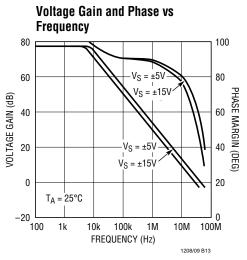


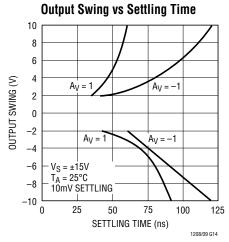
# TYPICAL PERFORMANCE CHARACTERISTICS

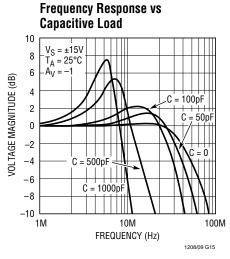


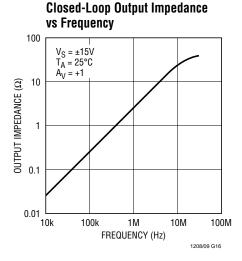


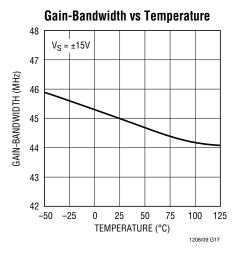


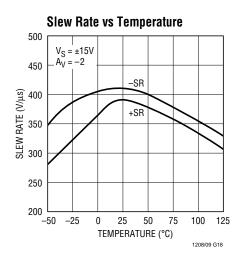






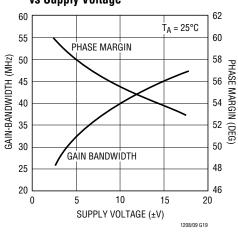




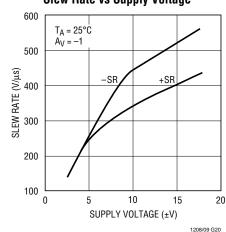


# TYPICAL PERFORMANCE CHARACTERISTICS

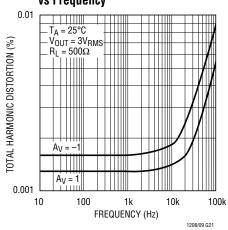
Gain-Bandwidth and Phase Margin vs Supply Voltage



Slew Rate vs Supply Voltage



**Total Harmonic Distortion** vs Frequency



# APPLICATIONS INFORMATION

# **Layout and Passive Components**

As with any high speed operational amplifier, care must be taken in board layout in order to obtain maximum performance. Key layout issues include: use of a ground plane, minimization of stray capacitance at the input pins, short lead lengths, RF-quality bypass capacitors located close to the device (typically 0.01µF to 0.1µF), and use of low ESR bypass capacitors for high drive current applications (typically 1µF to 10µF tantalum). Sockets should be avoided when maximum frequency performance is reguired, although low profile sockets can provide reasonable performance up to 50MHz. For more details see Design Note 50. The parallel combination of the feedback resistor and gain setting resistor on the inverting input combine with the input capacitance to form a pole which can cause peaking. If feedback resistors greater than 5k are used, a parallel capacitor of value

$$C_F \ge R_G \times C_{IN}/R_F$$

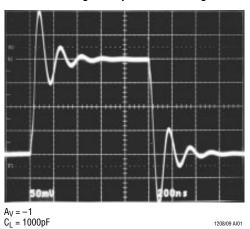
should be used to cancel the input pole and optimize dynamic performance. For unity-gain applications where a large feedback resistor is used, C<sub>F</sub> should be greater than or equal to C<sub>IN</sub>.

# **Capacitive Loading**

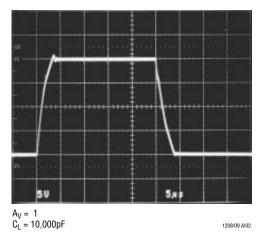
The LT1208/LT1209 amplifiers are stable with capacitive loads. This is accomplished by sensing the load induced output pole and adding compensation at the amplifier gain node. As the capacitive load increases, both the bandwidth and phase margin decrease so there will be peaking in the frequency domain and in the transient response. The photo of the small-signal response with 1000pF load shows 50% peaking. The large-signal response with a 10,000pF load shows the output slew rate being limited by the short-circuit current. To reduce peaking with capacitive loads, insert a small decoupling resistor between the output and the load, and add a capacitor between the output and inverting input to provide an AC feedback path. Coaxial cable can be driven directly, but for best pulse fidelity the cable should be doubly terminated with a resistor in series with the output.

# APPLICATIONS INFORMATION

# **Small-Signal Capacitive Loading**



**Large-Signal Capacitive Loading** 



# **Input Considerations**

Resistors in series with the inputs are recommended for the LT1208/LT1209 in applications where the differential input voltage exceeds ±6V continuously or on a transient basis. An example would be in noninverting configurations with high input slew rates or when driving heavy capacitive loads. The use of balanced source resistance at each input is recommended for applications where DC accuracy must be maximized.

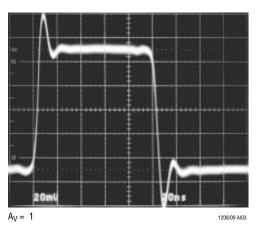
# Transient Response

The LT1208/LT1209 gain-bandwidth is 45MHz when measured at 100kHz. The actual frequency response in unitygain is considerably higher than 45MHz due to peaking

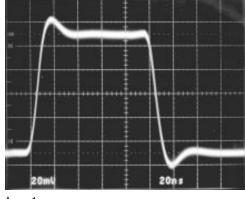
caused by a second pole beyond the unity-gain crossover. This is reflected in the 50° phase margin and shows up as overshoot in the unity-gain small-signal transient response. Higher noise gain configurations exhibit less overshoot as seen in the inverting gain of one response.

The large-signal response in both inverting and non-inverting gain show symmetrical slewing characteristics. Normally the noninverting response has a much faster rising edge due to the rapid change in input common-mode voltage which affects the tail current of the input differential pair. Slew enhancement circuitry has been added to the LT1208/LT1209 so that the falling edge slew rate is balanced.

**Small-Signal Transient Response** 



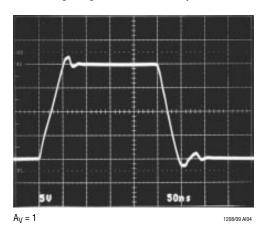
**Small-Signal Transient Response** 



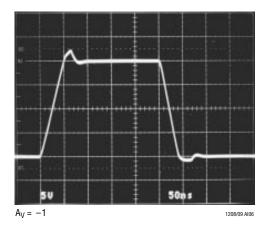
 $A_V = -1$  1208/09 AIO4

# APPLICATIONS INFORMATION

**Large-Signal Transient Response** 



**Large-Signal Transient Response** 



# **Low Voltage Operation**

The LT1208/LT1209 are functional at room temperature with only 3V of total supply voltage. Under this condition, however, the undistorted output swing is only  $0.8V_{P-P}$ . A more realistic condition is operation at  $\pm 2.5V$  supplies (or 5V and ground). Under these conditions, at room temperature, the typical input common-mode range is 1.9V to -1.3V (for a  $V_{OS}$  change of 1mV), and a 5MHz,  $2V_{P-P}$  sine wave can be faithfully reproduced. With 5V total supply voltage the gain-bandwidth is reduced to 26MHz and the slew rate is reduced to  $135V/\mu s$ .

# **Power Dissipation**

The LT1208/LT1209 combine high speed and large output current drive in small packages. Because of the wide supply voltage range, it is possible to exceed the maximum junction temperature under certain conditions.

Maximum junction temperature  $(T_J)$  is calculated from the ambient temperature  $(T_A)$  and power dissipation  $(P_D)$  as follows:

 $\begin{array}{ll} LT1208CN8: & T_J = T_A + (P_D \times 100^{\circ} C/W) \\ LT1208CS8: & T_J = T_A + (P_D \times 150^{\circ} C/W) \\ LT1209CN: & T_J = T_A + (P_D \times 70^{\circ} C/W) \\ LT1209CS: & T_J = T_A + (P_D \times 100^{\circ} C/W) \end{array}$ 

Maximum power dissipation occurs at the maximum supply current and when the output voltage is at 1/2 of either supply voltage (or the maximum swing if less than 1/2 supply voltage).

For each amplifier P<sub>DMAX</sub> is as follows:

$$P_{DMAX} = (V^+ - V^-)(I_{SMAX}) + \frac{(0.5V^+)^2}{R_L}$$

Example: LT1208 in S8 at 70°C,  $V_S = \pm 10V$ ,  $R_L = 500\Omega$ 

$$P_{\text{DMAX}} = (20\text{V})(10.5\text{mA}) + \frac{(5\text{V})^2}{500\Omega} = 260\text{mW}$$

$$T_J = 70^{\circ}\text{C} + (2 \times 260\text{mW})(150^{\circ}\text{C/W}) = 148^{\circ}\text{C}$$

# **DAC Current-to-Voltage Converter**

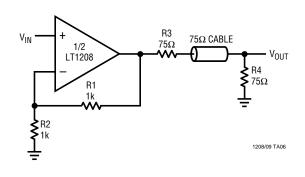
The wide bandwidth, high slew rate and fast settling time of the LT1208/LT1209 make them well-suited for current-to-voltage conversion after current output D/A converters. A typical application with a DAC-08 type converter (full-scale output of 2mA) uses a 5k feedback resistor. A 7pF compensation capacitor across the feedback resistor is used to null the pole at the inverting input caused by the DAC output capacitance. The combination of the LT1208/LT1209 and DAC settles to less than 40mV (1LSB) in 140ns for a 10V step.

# TYPICAL APPLICATIONS

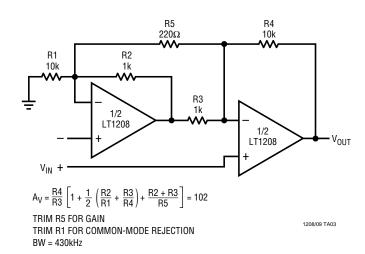
# **DAC Current-to-Voltage Converter**

# DAC-08 TYPE 1/2 LT1208 1 LSB SETTLING = 140ns 1208/09 ΤΑΟ4

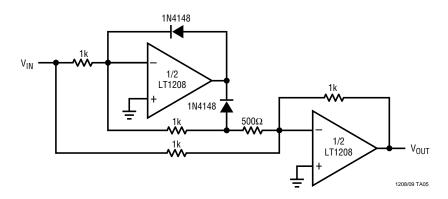
# **Cable Driving**



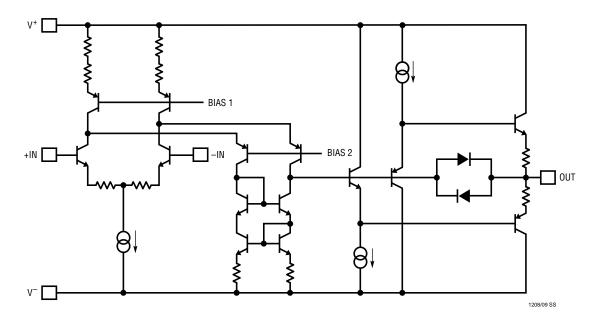
# **Instrumentation Amplifier**



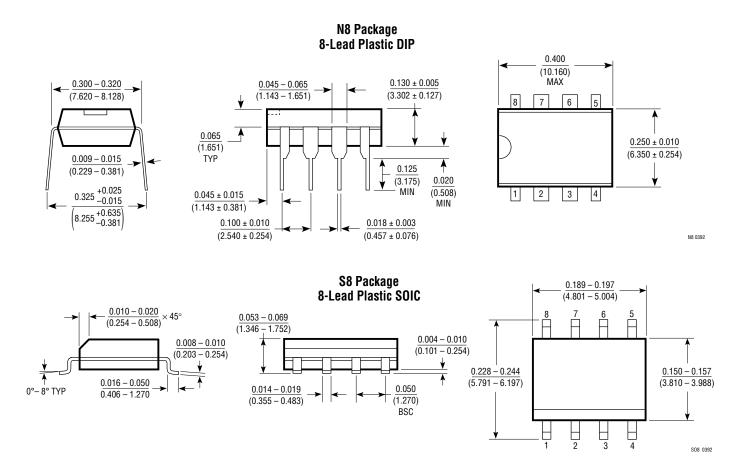
# **Full-Wave Rectifier**



# SIMPLIFIED SCHEMATIC

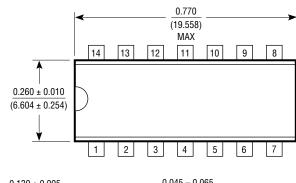


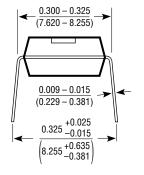
# PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

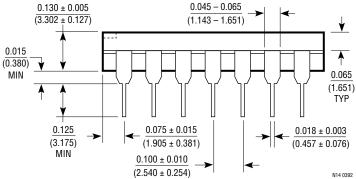


# PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

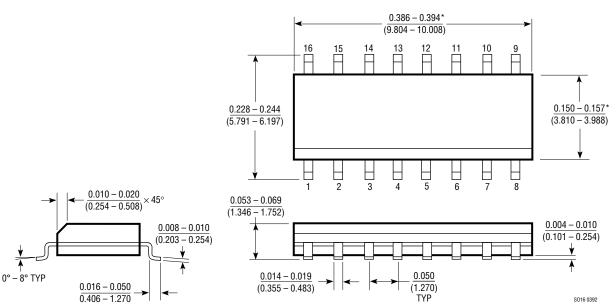
### N Package 14-Lead Plastic DIP







# S Package 16-Lead Plastic SOIC



# NORTHEAST REGION Linear Technology Corporation

One Oxford Valley 2300 E. Lincoln Hwy.,Suite 306 Langhorne, PA 19047 Phone: (215) 757-8578 FAX: (215) 757-5631

### **Linear Technology Corporation**

266 Lowell St., Suite B-8 Wilmington, MA 01887 Phone: (508) 658-3881 FAX: (508) 658-2701

# U.S. Area Sales Offices

# SOUTHEAST REGION Linear Technology Corporation

17060 Dallas Parkway Suite 208 Dallas, TX 75248

Phone: (214) 733-3071 FAX: (214) 380-5138

# **CENTRAL REGION**

# **Linear Technology Corporation**

Chesapeake Square 229 Mitchell Court, Suite A-25 Addison, IL 60101

Phone: (708) 620-6910 FAX: (708) 620-6977

# SOUTHWEST REGION

**Linear Technology Corporation** 22141 Ventura Blvd.

Suite 206

Woodland Hills, CA 91364 Phone: (818) 703-0835 FAX: (818) 703-0517

### NORTHWEST REGION Linear Technology Corporation

782 Sycamore Dr. Milpitas, CA 95035 Phone: (408) 428-2050 FAX: (408) 432-6331

### **International Sales Offices**

### **FRANCE**

### Linear Technology S.A.R.L.

Immeuble "Le Quartz"
58 Chemin de la Justice
92290 Chatenay Malabry
France

Phone: 33-1-41079555 FAX: 33-1-46314613

### **GERMANY**

### **Linear Techonolgy GMBH**

Untere Hauptstr. 9 D-8057 Eching Germany

Phone: 49-89-3197410 FAX: 49-89-3194821

### **JAPAN**

# Linear Technology KK

5F YZ Bldg.

lidabashi, Chiyoda-Ku Tokyo, 102 Japan Phone: 81-3-3237-7891 FAX: 81-3-3237-8010

### **KOREA**

### Linear Technology Korea Branch

Namsong Building, #505 Itaewon-Dong 260-199 Yongsan-Ku, Seoul Korea

Phone: 82-2-792-1617 FAX: 82-2-792-1619

### **SINGAPORE**

### Linear Technology Pte. Ltd.

101 Boon Keng Road #02-15 Kallang Ind. Estates

Singapore 1233 Phone: 65-293-5322 FAX: 65-292-0398

### **TAIWAN**

# **Linear Technology Corporation**

Rm. 801, No. 46, Sec. 2 Chung Shan N. Rd. Taipei, Taiwan, R.O.C. Phone: 886-2-521-7575 FAX: 886-2-562-2285

### **UNITED KINGDOM**

# Linear Technology (UK) Ltd.

The Coliseum, Riverside Way Camberley, Surrey GU15 3YL

United Kingdom Phone: 44-276-677676 FAX: 44-276-64851

# **World Headquarters**

### **Linear Technology Corporation**

1630 McCarthy Blvd. Milpitas, CA 95035-7487 Phone: (408) 432-1900 FAX: (408) 434-0507

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