

Approximate Minimization Using Newton's Method:

For a point u^i , $P_{app}(u) = f(u^i) + (u - u^i)^T \frac{\partial f}{\partial u} + \frac{1}{2}(u - u^i)^T H(u - u^i)$

Newton's Method: $H(u^{i+1} - u^i) = -\frac{\partial f}{\partial u}(u^i)$

As $u^i \rightarrow u^*$, $\frac{\partial f}{\partial u} = 0$.

Numerical Linear Algebra:

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We seek to solve systems:

$$Ku = f, \quad Kx = \lambda x, \quad Mu'' + Ku = 0.$$

1. Elimination: $A = LU$ Lower Triangular
Upper Triangular
2. Orthogonalization: $A = QR$ orthogonal columns
upper triangular
3. Singular Value Decomposition:

$$A = U \Sigma V^T$$

↑ ↗ ↘
orthonormal columns singular values orthonormal rows

For a pos. def. K , $U = Q$ and $V^T = Q^T$, $\Sigma = \Lambda$.

Orthogonal Matrices:

Let $Q = [q_1 \dots q_n]$, $q_i^T q_j = 0$ if $i \neq j$, $q_i^T q_i = 1$

$$\Rightarrow Q^T Q = I.$$

For Q a square matrix $Q^{-1} = Q^T$.

$$\bullet \|Qx\| = \|x\|,$$

Indeed, $\|Qx\|^2 = x^T Q^T Q x = x^T x = \|x\|^2$

Examples: Permutations, Rotations, Reflections

$$\bullet \begin{bmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} y \\ x \\ z \end{bmatrix}$$

$$P^T P = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} = I.$$

$$\bullet Q = \begin{bmatrix} \cos \theta & 0 & -\sin \theta \\ 0 & 1 & 0 \\ \sin \theta & 0 & \cos \theta \end{bmatrix}$$

Rotation in the
1-3 plane

$$\bullet H = \begin{bmatrix} -\cos(2\theta) & 0 & -\sin(2\theta) \\ 0 & 1 & 0 \\ -\sin(2\theta) & 0 & \cos(2\theta) \end{bmatrix} = I - 2nn^T$$

for $n \perp$ to the plane of reflection, $n = (\cos \theta, 0, \sin \theta)$

Orthogonalization $A = QR$: Take A an $m \times n$ matrix with n linearly independent columns $a_1, \dots, a_n$.

1. Gram-Schmidt Algorithm:

Ex. $\begin{bmatrix} a_1 & a_2 \end{bmatrix} = \begin{bmatrix} g_1 & g_2 \end{bmatrix} \begin{bmatrix} r_{11} & r_{12} \\ 0 & r_{22} \end{bmatrix}$ Set $g_1 = \frac{a_1}{\|a_1\|}$

Take $B_2 = a_2 - (g_1^T a_2) g_1$ s.t. $B_2 \perp g_1$.

$$\text{Set } g_2 = \frac{B_2}{\|B_2\|}$$

$$\vdots$$

$$B_n = a_n - (g_1^T a_n) g_1 - \dots - (g_{n-1}^T a_n) g_{n-1},$$

$$\text{Set } g_n = \frac{B_n}{\|B_n\|}.$$

2. Householder Algorithm:

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$$[a_1, a_2] = [q_1, q_2, q_3] \begin{bmatrix} r_{11} & r_{12} \\ 0 & r_{22} \end{bmatrix}$$

Matlab stores the QR decomposition in this form.

$$A = \begin{bmatrix} a_1 & \dots & a_n \end{bmatrix}$$

$$\Rightarrow u = a_1 - \alpha_1 e_1, \quad \alpha_1 = \frac{a_1^T a_1}{\|a_1\|} e^{i \arg(a_1)} \|a_1\|$$

$$\Rightarrow v = \frac{u}{\|u\|}$$

$$\Rightarrow Q_1 = I - 2vv^T$$

$$\Rightarrow Q_1 A = \begin{bmatrix} \alpha_1 & \dots & \dots \\ 0 & & \\ \vdots & & \\ 0 & & A' \end{bmatrix}$$

Repeat for A' .

$$Q = Q_1^T \dots Q_n^T$$

Singular Value Decomposition:

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For a symmetric matrix A , $A = S \Lambda S^{-1}$.

Otherwise, $A = U \Sigma V^T$, where Σ now contains singular values instead of eigen values:

$$\begin{aligned} A^T A &= (U \Sigma V^T)^T (U \Sigma V^T) = V \Sigma^T U^T U \Sigma V^T \\ &= V \underbrace{\Sigma^T \Sigma}_{\substack{\uparrow \\ \text{diagonal}}} V^T \end{aligned}$$

Find:

$$A^T A v_i = \sigma_i^2 v_i$$

We want $AV = U\Sigma$, so we

need $u_i = \frac{Av_i}{\sigma_i}$. Let $v_1, \dots, v_r$ be the basis for $CS(A)$,
 $u_1, \dots, u_r$ the basis for $RS(A)$.

Reduced SVD: $A = U_{m \times r} \Sigma_{r \times r} V_{r \times n}^T$

$$= \begin{bmatrix} u_1 & \dots & u_r \end{bmatrix} \begin{bmatrix} \sigma_1 & & 0 \\ & \ddots & \\ 0 & & \sigma_r \end{bmatrix} \begin{bmatrix} v_1^T \\ \vdots \\ v_r^T \end{bmatrix}$$

To complete the process, add any orthonormal basis $v_{r+1}, \dots, v_n$ for the nullspace of A ; $u_{r+1}, \dots, u_m$ an orthonormal basis for the nullspace of A^T .

Full SVD: $A = U_{m \times m} \Sigma_{m \times n} V_{n \times n}^T =$

$$\begin{bmatrix} u_1 & \dots & u_m \end{bmatrix} \begin{bmatrix} \sigma_1 & & \\ & \ddots & \\ & & \sigma_r \end{bmatrix} \begin{bmatrix} v_1^T \\ \vdots \\ v_n^T \end{bmatrix}$$

Ordering u_i, σ_i, v_i s.t. $\sigma_1 \geq \sigma_2 \geq \dots \geq \sigma_r$.

$$A = \underset{\substack{\uparrow \\ \text{largest}}}{u_1} \sigma_1 \underset{\substack{\uparrow \\ \text{smallest}}}{v_1^T} + \dots + u_r \sigma_r v_r^T$$

SVD: $Av_j = \sigma_j u_j$ for $j \leq r$ $A^T u_j = \sigma_j v_j$ for $j \leq r$ (25)
 $Av_j = 0$ for $j > r$ $A^T u_j = 0$ for $j > r$

For a symmetric, pos. def K , $v_i = u_i$.

V is a rotation, Σ is a rescaling, U a rotation.

Start with $A^T A v_i = \sigma_i^2 v_i$

$$\Rightarrow v_i^T A^T A v_i = \sigma_i^2 v_i^T v_i \Rightarrow \|A v_i\| = \sigma_i \Rightarrow \|u_i\| = 1$$

$$\Rightarrow v_j^T A^T A v_i = \sigma_i^2 v_j^T v_i \Rightarrow (A v_j) \cdot (A v_i) = 0 \Rightarrow u_j^T u_i = 0$$

$$\Rightarrow A A^T (A v_i) = \sigma_i^2 A v_i \Rightarrow A A^T u_i = \sigma_i^2 u_i$$

Ex: Find the SVD for $A = \begin{bmatrix} 1 & 1 \\ 7 & 7 \end{bmatrix}$. (Rank 1)

$$A^T A = \begin{bmatrix} 50 & 50 \\ 50 & 50 \end{bmatrix} \text{ has e.v.'s } \lambda = 100, 0; v_1 = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \frac{1}{\sqrt{2}} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

$$\Rightarrow u_1 = \frac{A v_1}{10} = \frac{1}{\sqrt{50}} \begin{bmatrix} 1 \\ 7 \end{bmatrix}, u_2 = \frac{1}{\sqrt{50}} \begin{bmatrix} -7 \\ 1 \end{bmatrix}$$

$$\Rightarrow A = U \Sigma V^T = \frac{1}{\sqrt{50}} \begin{bmatrix} 1 & -7 \\ 7 & 1 \end{bmatrix} \begin{bmatrix} 10 & 0 \\ 0 & 0 \end{bmatrix} \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

Pseudoinverse:

$$A^+ = V \Sigma^+ U^T, \quad A^+ u_i = \frac{v_i}{\sigma_i} \text{ for } i \leq r,$$

$$A^+ u_i = 0 \text{ for } i > r.$$

The pseudoinverse has the same rank r as A .

$$\Sigma^+ = \begin{bmatrix} \sigma_1^{-1} & & 0 \\ & \ddots & \\ 0 & & \sigma_r^{-1} & 0 \\ & & & 0 \end{bmatrix}, \quad \Sigma^+ \Sigma \text{ as close to Id as possible.}$$

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$$AA^+ = \text{Projection onto } CS(A),$$

$$A^+A = \text{Proj. onto } RS(A).$$

Ex: The pseudoinverse of $A = \begin{bmatrix} 1 & 1 \\ 7 & 7 \end{bmatrix}$ is

$$\begin{aligned} A^+ &= U \Sigma^+ U^T = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & -1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} \frac{1}{10} & 0 \\ 0 & 0 \end{bmatrix} \frac{1}{\sqrt{20}} \begin{bmatrix} 1 & 7 \\ -7 & 1 \end{bmatrix} \\ &= \frac{1}{100} \begin{bmatrix} 1 & 7 \\ 1 & 7 \end{bmatrix}. \end{aligned}$$

If $b \in CS(A)$, $Ax=b$ is solvable and A^+b is the shortest solution.

Condition Numbers and Norms:

The condition # of a symmetric matrix is

$$c(K) = \frac{\lambda_{\max}}{\lambda_{\min}}.$$

This measures the sensitivity of the system $Ku=f$ to changes. Let $K_0 = K$, $K(u+\Delta u) = f + \Delta f$

$$\Rightarrow \Delta u = K^{-1}(\Delta f)$$

$$\Rightarrow \|\Delta u\| \leq \frac{\|\Delta f\|}{\lambda_{\min}(K)}.$$

$\lambda_{\max}(K^{-1}) = \frac{1}{\lambda_{\min}(K)}$. The eigenvalue $\lambda_{\min}$ measures the closeness of K to being singular, but there are 2 drawbacks to only using this as a measure:

• $1000 \cdot K \left(\frac{n}{1000} \right) = A$ but $\frac{\|DA\|}{\|n\|}$ does not change.

We have:

$$\text{Provide } \|DA\| \leq \frac{\|DA\|}{\lambda_{\min}(K)} \text{ by } \|n\| \geq \frac{\|A\|}{\lambda_{\max}(K)}$$
$$\Rightarrow \frac{\|DA\|}{\|n\|} \leq \frac{\lambda_{\max}(K)}{\lambda_{\min}(K)} \frac{\|A\|}{\|A\|}$$

$\Rightarrow$ A is largest when DA an eigenvector for $\lambda_{\min}$,
is smallest when A an eigenvector for $\lambda_{\max}$.

When A not symmetric, $\|Ax\| \leq \lambda_{\max}(A) \|x\|$ can break down.
 $\Rightarrow$ Other vectors can blow-up more than eigenvectors.

Ex: $A = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$, $A^T A = \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$, $\|A\| = \frac{1+\sqrt{5}}{2}$, e.v.'s = 1

~~(e.v.'s = 1)~~
 ~~$\|A\| = \frac{1+\sqrt{5}}{2}$~~

$\|A\|^2 = \lambda_{\max}(A^T A) \approx 2.6$, $\frac{1}{\|A^{-1}\|^2} = \lambda_{\min}(A^T A) \approx \frac{1}{2.6} \Rightarrow \|A\| \|A^{-1}\| \approx 2.6$

Def: Norm $\|A\| = \max_{x \neq 0} \frac{\|Ax\|}{\|x\|}$, Condition #: $c(A) = \|A\| \|A^{-1}\|$

For matrix norms, we have:

$$\|Ax\| \leq \|A\| \|x\|, \|AB\| \leq \|A\| \|B\|, \|A+B\| \leq \|A\| + \|B\|.$$

$1000 A$ has norm $1000 \|A\|$ but $c_n(1000 A) = c_n(A)$.

For a positive definite matrix,

$$\|K\| = \lambda_{\max}(K).$$

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Indeed, $K = Q\Lambda Q^T$ leaves lengths unchanged $\Rightarrow \|K\| = \|\Lambda\| = \lambda_{\max}(K)$.

Similarly, $\|K^{-1}\| = \frac{1}{\lambda_{\min}(K)} \Rightarrow c(K) = \frac{\lambda_{\max}}{\lambda_{\min}}.$

Ex: $Ax = \begin{bmatrix} 0 & 2 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 2 \\ 0 \end{bmatrix}, \quad \frac{\|Ax\|}{\|x\|} = 2.$

$A^T A = \begin{bmatrix} 0 & 0 \\ 0 & 4 \end{bmatrix} \Rightarrow \sigma_1^2 = 4 \Rightarrow \|A\| = 2 = \text{largest singular value.}$

The singular value $\sqrt{\lambda_{\max}(A^T A)}$ is generally larger than $\lambda_{\max}(A)$.

$$\|A\|^2 = \max \frac{\|Ax\|^2}{\|x\|^2} = \max \frac{x^T A^T A x}{x^T x} = \lambda_{\max}(A^T A) = \sigma_{\max}^2.$$

$$\Rightarrow c(A) = \|A\| \|A^{-1}\| = \frac{\sigma_{\max}}{\sigma_{\min}}.$$

Ex: $A = \begin{bmatrix} 1 & 7 \\ 0 & 1 \end{bmatrix}, \quad A^{-1} = \begin{bmatrix} 1 & -7 \\ 0 & 1 \end{bmatrix}$

$\Rightarrow c(A) = \|A\| \|A^{-1}\|$ is at least $\sqrt{50} \sqrt{50} = 50$:

$Ax = \begin{bmatrix} 1 & 7 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 7 \\ 1 \end{bmatrix}$ has $\frac{\|Ax\|}{\|x\|} = \sqrt{50} \Rightarrow \|A\| \geq \sqrt{50}$

$A^{-1}x = \begin{bmatrix} 1 & -7 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} -7 \\ 1 \end{bmatrix}$ has $\frac{\|A^{-1}x\|}{\|x\|} = \sqrt{50} \Rightarrow \|A^{-1}\| \geq \sqrt{50}$

$$\Rightarrow \frac{\|Dx\|}{\|x\|} = .1 \sqrt{50}, \quad \frac{\|D^{-1}b\|}{\|b\|} = \frac{1}{.1 \sqrt{50}}$$

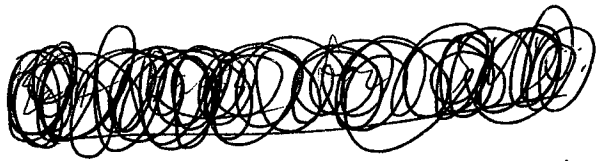
$$2. \quad c(K_n) = \|K\| \|K^{-1}\| = \frac{\lambda_{\max}}{\lambda_{\min}} = \frac{2 - 2\cos \frac{n\pi}{n+1}}{2 - 2\cos \frac{\pi}{n+1}} \approx \frac{4}{\pi^2} (n+1)^2$$

In computation, there is a log c loss to round off error.

Row Exchanges in $PA=LU$:

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To determine the usefulness of an algorithm early on, sometimes it is necessary to re-order rows so that the largest pivot entry. Partial pivoting avoids multipliers in L larger than 1.



Equilibrium and the Stiffness Matrix:

Often statics come in the form of the framework:

$$\begin{array}{ccccccc} & e = Au & , & w = Ce & , & f = A^T w & \\ \text{Physical} & \uparrow & & \uparrow & & \uparrow & \nwarrow \\ \text{Set-up} & \text{Displacements} & & \text{Spring} & & \text{force} & \text{Balancing:} \\ & & & \text{Tension} & & & \end{array}$$

$$\Rightarrow f = \underbrace{A^T C A} u$$

$K \equiv$ the stiffness matrix

Dynamics and Nonlinearity:

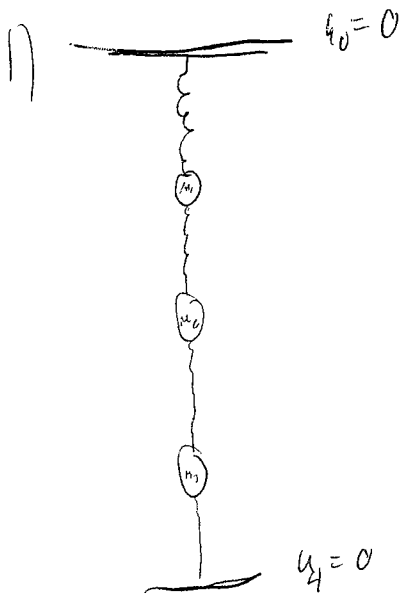
$K_h = A$ is the set-up for linear, static problems (equilibrium).

However, problems may have nonlinear components or be dynamic.

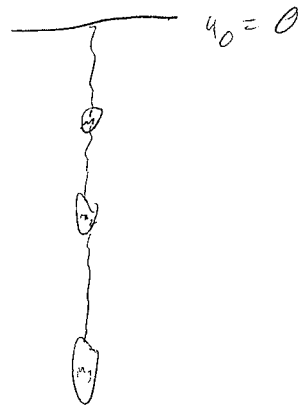
$$\Rightarrow \frac{dq}{dt} = K_h - f \quad \text{or} \quad M \frac{d^2 q}{dt^2} + K_h = f(t)$$

Springs:

The first application we explore will be for systems of springs.



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Define $\vec{u} = (u_1, u_2, u_3) \equiv$ mass displacements

$\vec{w} = (w_1, w_2, w_3, w_4)$ or $(w_1, w_2, w_3) \equiv$ tension in springs

Positive Displacement is downward.

Tension positive / Compression negative.

In this case, the spring constants c_i relate the tension to the stretching: $w_i = c_i e_i$ (Force = spring constant $\times$ elongation)

The forces are produced by gravity $(m_1 g, m_2 g, m_3 g)$

To construct K , we have:

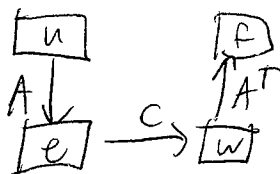
$u =$ Displacement of n masses $= (u_1, \dots, u_n)$

$e =$ Elongations of m springs $= (e_1, \dots, e_m)$

$w =$ Internal forces in m springs $= (w_1, \dots, w_m)$

$f =$ external forces on n masses $= (F_1, \dots, F_n)$

$\Rightarrow$



$$e = Au$$

$$A \quad n \times n$$

$$w = Ce$$

$$C \quad m \times m$$

$$f = A^T w$$

$$A^T \quad n \times m$$

First Spring: $e_1 = u_1$

Second Spring: $e_2 = u_2 - u_1$

Third Spring: $e_3 = u_3 - u_2$

Fourth Spring: $e_4 = -u_3$

Kinematic eqⁿ

$$\Rightarrow e = Au \quad \begin{bmatrix} e_1 \\ e_2 \\ e_3 \\ e_4 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \\ 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} u_1 \\ u_2 - u_1 \\ u_3 - u_2 \\ -u_3 \end{bmatrix}$$

Then, using Hooke's Law $\begin{bmatrix} w_1 \\ w_2 \\ w_3 \\ w_4 \end{bmatrix} = \begin{bmatrix} c_1 & 0 & 0 & 0 \\ 0 & c_2 & 0 & 0 \\ 0 & 0 & c_3 & 0 \\ 0 & 0 & 0 & c_4 \end{bmatrix} \begin{bmatrix} e_1 \\ e_2 \\ e_3 \\ e_4 \end{bmatrix} = Ce$ Constitutive Law

Finally, the internal forces w must balance the external forces f . Static equation.

$$\Rightarrow f_1 = w_1 - w_2$$

$$f_2 = w_2 - w_3$$

$$f_3 = w_3 - w_4$$

$\Rightarrow$

$$\begin{bmatrix} f_1 \\ f_2 \\ f_3 \end{bmatrix} = \begin{bmatrix} 1 & -1 & 0 & 0 \\ 0 & 1 & -1 & 0 \\ 0 & 0 & 1 & -1 \end{bmatrix} \begin{bmatrix} w_1 \\ w_2 \\ w_3 \\ w_4 \end{bmatrix}$$

$$\Rightarrow F = A^T w$$

$$\Rightarrow A^T C A u = F$$

Stiffness Matrix: For fixed ends,

$$K = \begin{bmatrix} c_1 + c_2 & -c_2 & 0 \\ -c_2 & c_2 + c_3 & -c_3 \\ 0 & -c_3 & c_3 + c_4 \end{bmatrix}$$

Note: $C = I$

$$\Rightarrow K = K_3$$

Similarly, if all springs are identical, $K = K_n$ for $n+1$ springs, (32)

Ex: $c_i = c, m_j = m \Rightarrow$

$$u = K^{-1}f = \frac{1}{4c} \begin{bmatrix} 3 & 2 & 1 \\ 2 & 4 & 2 \\ 1 & 2 & 3 \end{bmatrix} \begin{bmatrix} mg \\ mg \\ mg \end{bmatrix} = \frac{mg}{c} \begin{bmatrix} 1.5 \\ 2.0 \\ 1.5 \end{bmatrix} \quad \text{stretched}$$

$$e = Au = \begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \\ 0 & 0 & -1 \end{bmatrix} \frac{mg}{c} \begin{bmatrix} 1.5 \\ 2.0 \\ 1.5 \end{bmatrix} = \frac{mg}{c} \begin{bmatrix} 1.5 \\ 0.5 \\ -0.5 \\ -1.5 \end{bmatrix} \quad \text{unpressed}$$

It is not generally possible to compute

$$K^{-1} = A^{-1} C^{-1} (A^T)^{-1}$$

For a fixed end/free end problem:

$$A^T C A = \begin{bmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_1 & & 0 \\ & c_2 & \\ 0 & & c_3 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} c_1 + c_2 & -c_2 & 0 \\ -c_2 & c_2 + c_3 & -c_3 \\ 0 & -c_3 & c_3 \end{bmatrix}$$

For $C = I, \Rightarrow K = H_3$ which is T_3 with reversed ends.

Ex: $c_i = c, m_j = m \Rightarrow$

$$u = \frac{1}{c} \begin{bmatrix} 1 & 1 & 1 \\ 1 & 2 & 2 \\ 1 & 2 & 3 \end{bmatrix} \begin{bmatrix} mg \\ mg \\ mg \end{bmatrix} = \frac{mg}{c} \begin{bmatrix} 3 \\ 5 \\ 6 \end{bmatrix}$$

$$\Rightarrow e = \begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \end{bmatrix} \frac{mg}{c} \begin{bmatrix} 3 \\ 5 \\ 6 \end{bmatrix} = \frac{mg}{c} \begin{bmatrix} 3 \\ 2 \\ 1 \end{bmatrix}$$

$$\Rightarrow w = (A^T)^{-1} f = \begin{bmatrix} 1 & 1 & 1 \\ 0 & 1 & 1 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} mg \\ mg \\ mg \end{bmatrix} = \begin{bmatrix} 3mg \\ 2mg \\ mg \end{bmatrix}$$

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In this square case, $(A^T(A))^{-1} = (A^{-1}C^T(A^T)^{-1})$

Ex 1 Free-Free.

$$\begin{bmatrix} e_2 \\ e_3 \end{bmatrix} = \begin{bmatrix} u_2 - u_1 \\ u_3 - u_2 \end{bmatrix} = \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$



A singular

$\begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}$ represents the free shift operator that moves masses without stretching springs.

$$\Rightarrow \begin{bmatrix} -1 & 0 \\ 1 & -1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} c_2 & 0 \\ 0 & c_3 \end{bmatrix} \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 1 \end{bmatrix} = \begin{bmatrix} c_2 & -c_2 & 0 \\ -c_2 & c_2 + c_3 & -c_3 \\ 0 & -c_3 & c_3 \end{bmatrix}$$

Minimum Principles:

For a solution to $Ku = F$, we minimize the total potential energy:

$$P(u) = \frac{1}{2} u^T K u - u^T F$$

Nature seeks to minimize the total energy

Stretching increases internal energy $\frac{1}{2} e^T c e = \frac{1}{2} u^T K u$.

Masses lose potential energy by $F^T u$

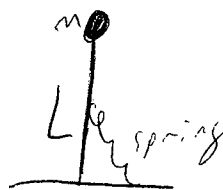
$$\text{Recall: } P(u) = \frac{1}{2} u^T K u - u^T F = \frac{1}{2} (u - K^{-1}F)^T K (u - K^{-1}F) - \frac{1}{2} F^T K^{-1} F$$

$$P_{\min} = -\frac{1}{2} F^T K^{-1} F \quad \text{at } u = K^{-1}F.$$

$P_{\min}$ negative because the masses lose potential energy when displaced.

Ex: Inverted Pendulum

$$P = \frac{1}{2} c \theta^2 + m g L \cos \theta$$



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$$\frac{dP}{d\theta} = c\theta - m g L \sin \theta = 0 \Rightarrow \text{crit. points (including } \theta=0)$$

$$\frac{d^2P}{d\theta^2} = c - m g L \cos \theta > 0 \text{ for stability}$$

$$\Rightarrow \text{stable at } \theta=0 \text{ if } c > m g L$$

$$\text{If } c < m g L, \text{ stable at } m g L \sin \theta^* = c \theta^*, \theta^* \neq 0.$$

2/4/2010

Oscillation Using Newton's Law

$$M_{\text{eff}} = f - K_n \Rightarrow M_{\text{eff}} + K_n = f.$$